


**Thermal Metric Project**

**Westford Symposium**  
2011.08.03

C. J. Schumacher  
Building Science Corporation




**Outline**

- Objective
- Approach
  - Apparatus:
    - Double Guarded Hot Box
  - Method:
    - 3 key elements
- Some Results
- Test Program
- Lessons

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**Objectives**

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**The Goal: a new metric**

- Develop a thermal performance rating system or **metric** that provides a means of crediting 'properly' built assemblies while penalizing 'poorly' built assemblies (of all types)

Means of crediting assemblies with good thermal control (materials, system design & construction quality)

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## What about the old metric?

### R-Value

- ❑ Property of a material
- ❑ Measurement of resistance to heat flow
- ❑ Proposed in 1945 by Everett Schuman, Penn State's Housing Research Institute



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## Benefits of R-Value

- ❑ Widely Accepted
  - ❑ FTC Regulation
- ❑ Simple to Measure
  - ❑ Commercially available test machines
- ❑ Easy to Communicate
  - ❑ ONE Number at standard temperature
  - ❑ Lumps all 3 modes of heat transfer into an *effective* conductivity
    - Conduction
    - Convection
    - Radiation



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## R-value Survey

Assume R30 insulation

Does insulation R-value change with outdoor temperature?

YES  
or  
NO

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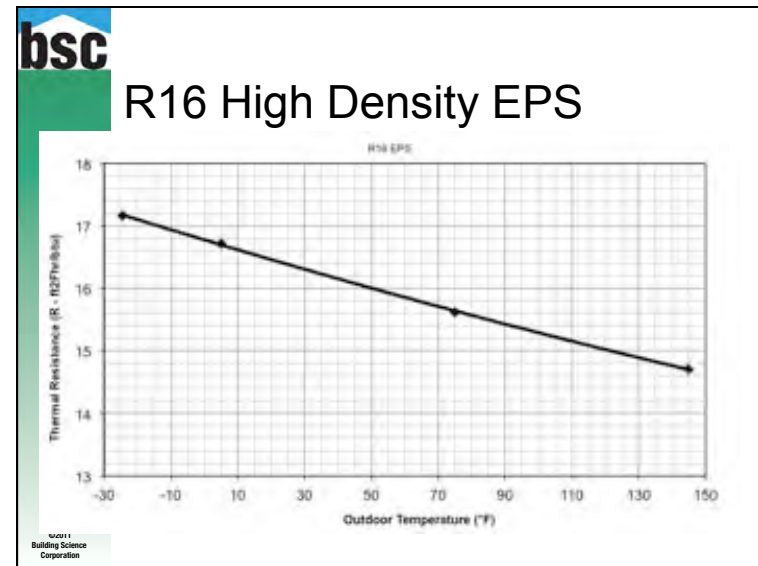
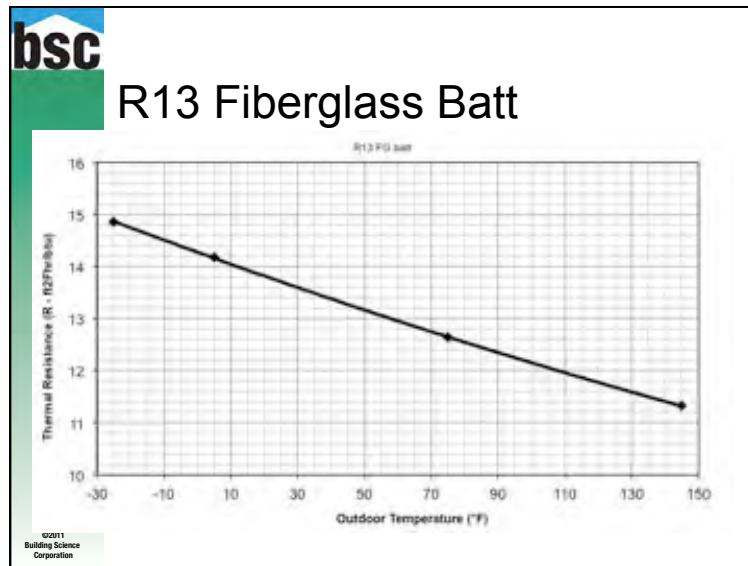
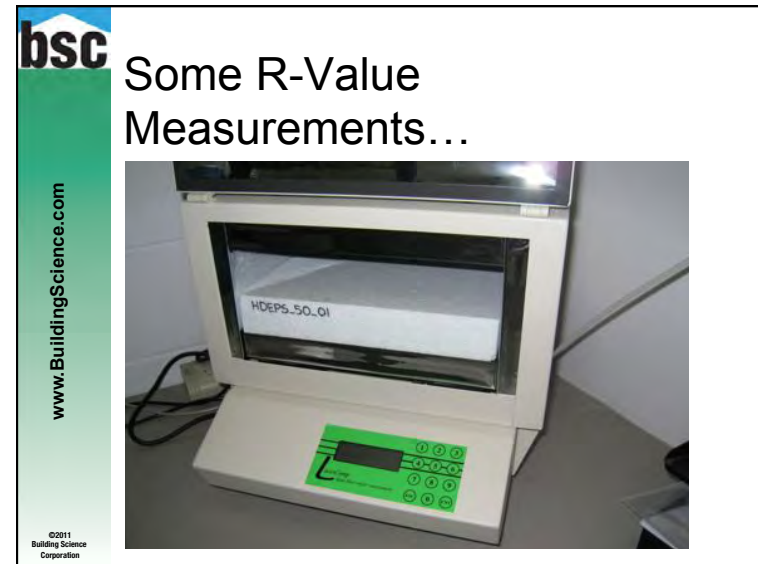
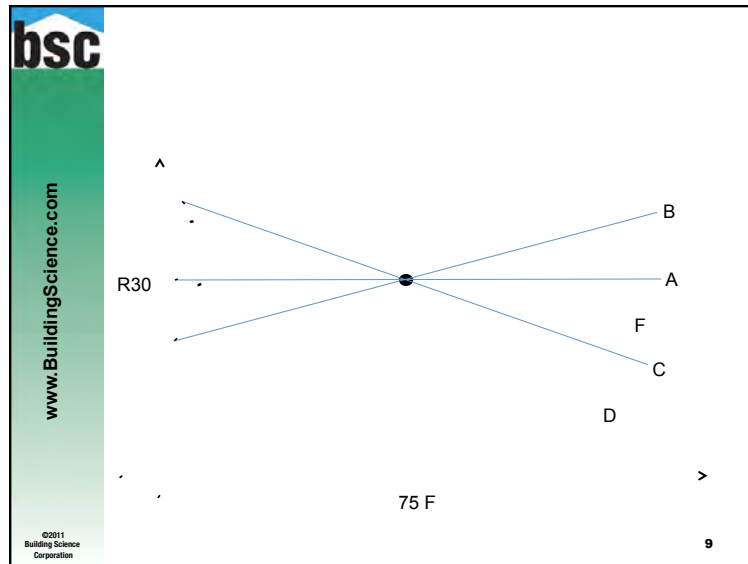
## R-value Survey (pt 2)

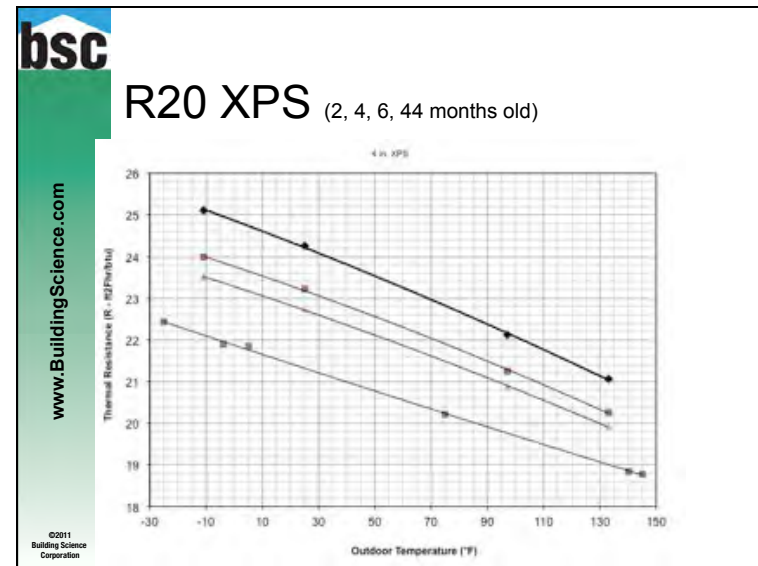
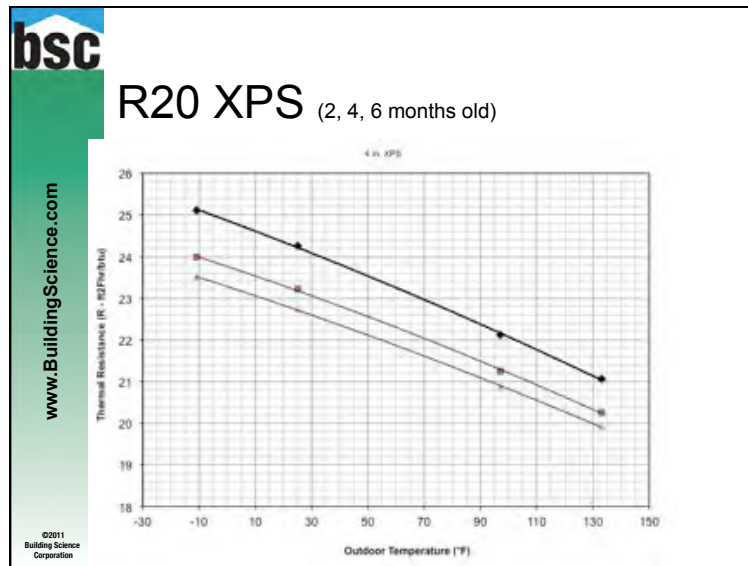
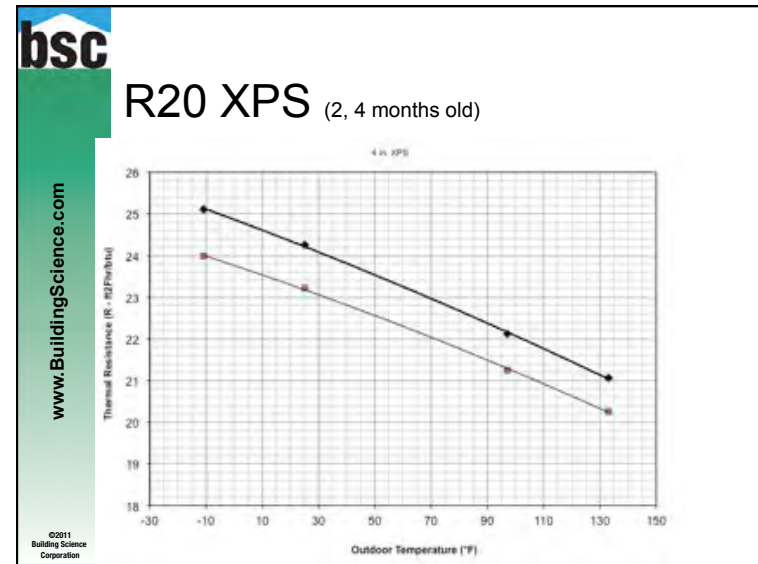
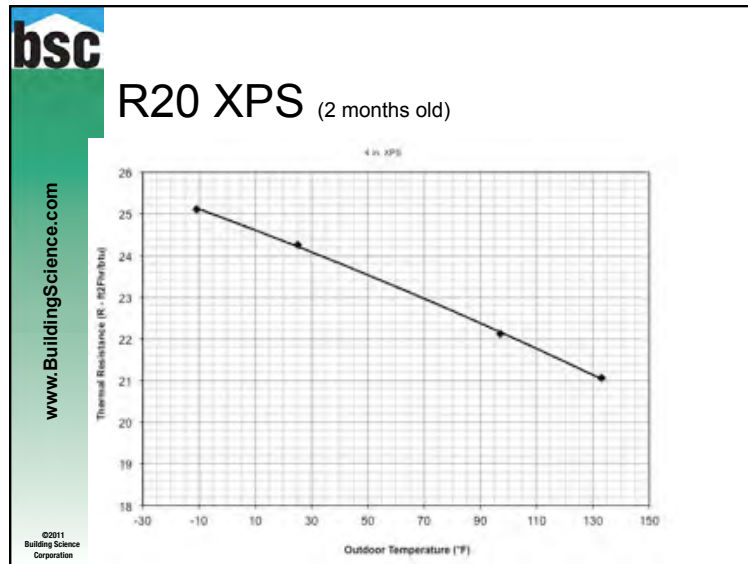
As the outdoor temperature decreases does the R-value:

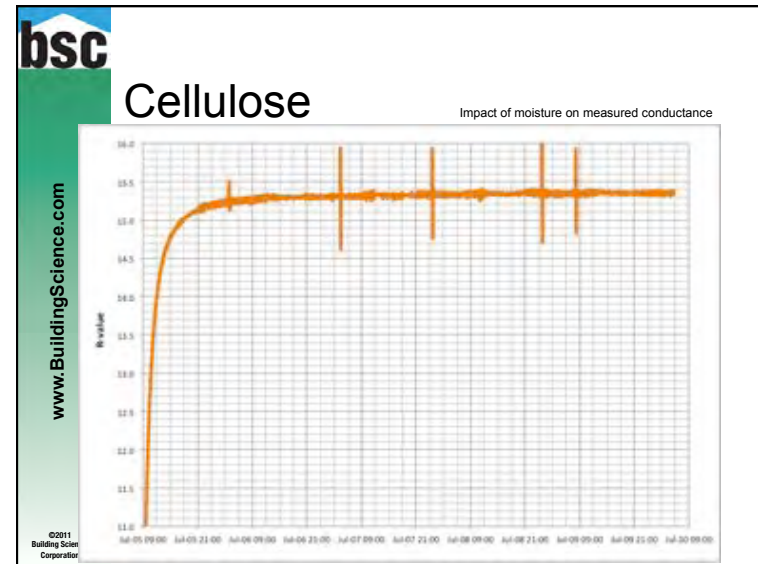
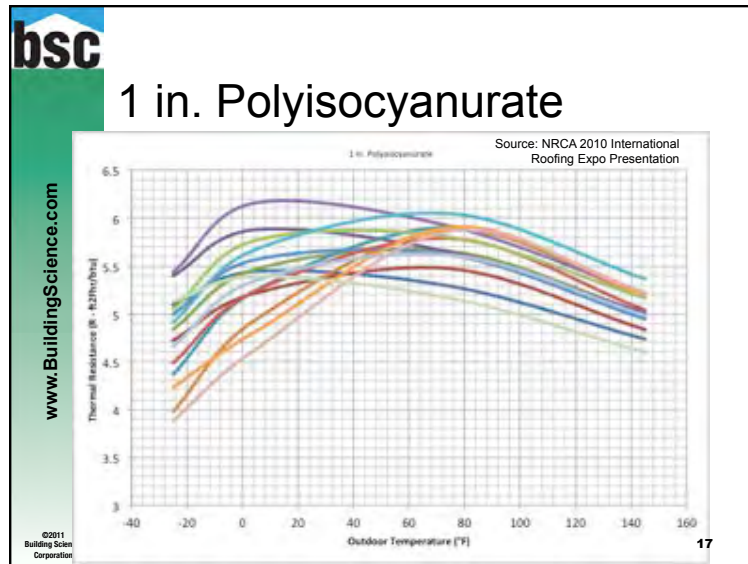
1. Increase
2. Decrease
3. Both 1 & 2
4. None of the above
5. I don't know, I'm still thinking about the BBQ & beer

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## Limitations of R-Value

- ❑ Definition implies thermal performance is constant
- ❑ Only true if
  - ❑ *Effective* conductivity is constant
  - ❑ No temperature sensitivity
  - ❑ No airflow sensitivity
  - ❑ No moisture adsorption
  - ❑ Material is homogenous
- ❑ Reasonable for *some* materials
- ❑ Not reasonable for most *real* building assemblies under *real* conditions

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## To develop a new metric

- ❑ Characterize *in-service* thermal performance
- ❑ Full-scale wood frame wall assemblies
- ❑ Realistic boundary conditions

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## Approach

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## Approach

- Research work required the development of new apparatus:
  - a different type of Hot Box
- new methods:
  - unique wall specimens
  - control of extra boundary conditions
  - measurement of extra variables

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## Industry Partners

- Dow
- Greenfiber
- Honeywell
- Huntsman Polyurethanes
- Icynene Insulation System
- NAIMA (Certainteed & Johns Manville)

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# Apparatus

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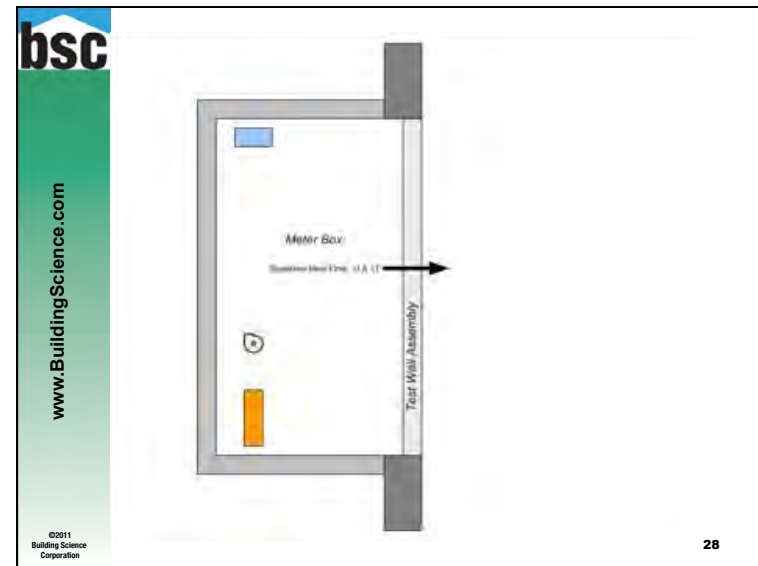
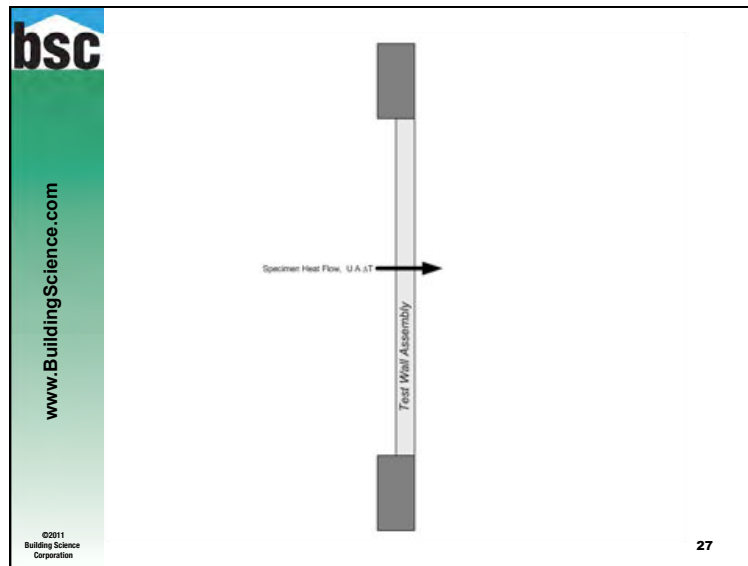
## A Double Guarded Hot Box

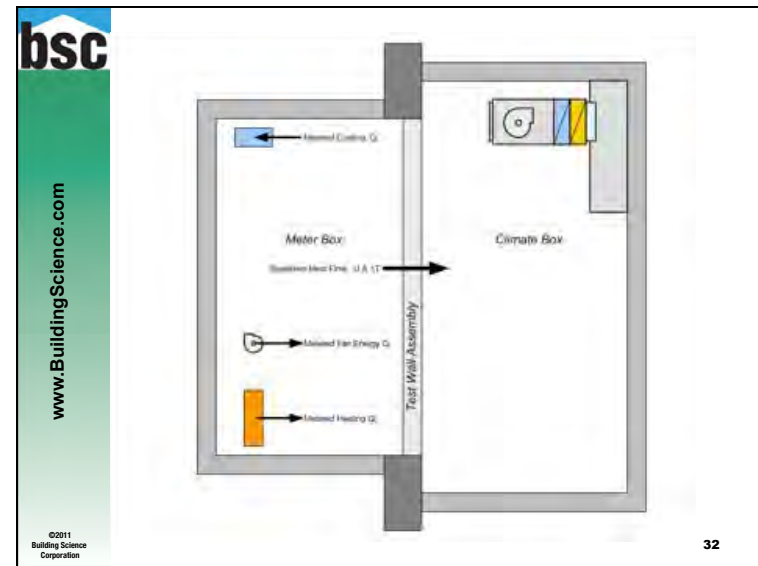
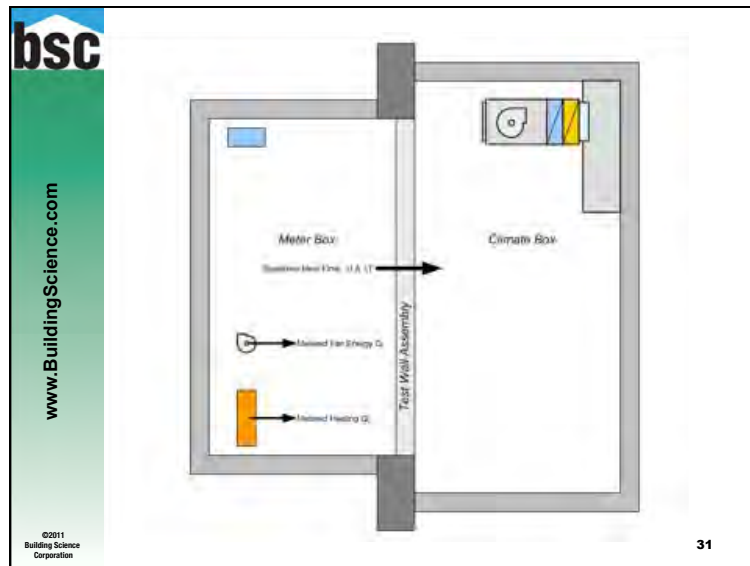
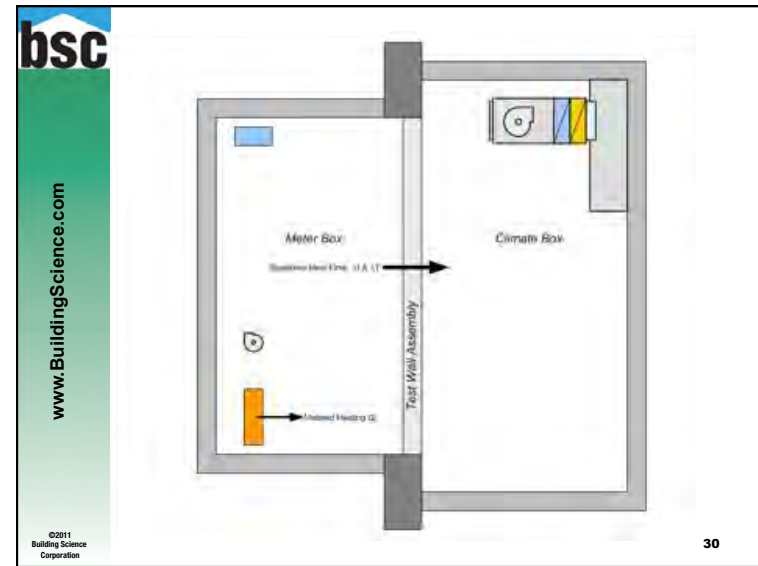
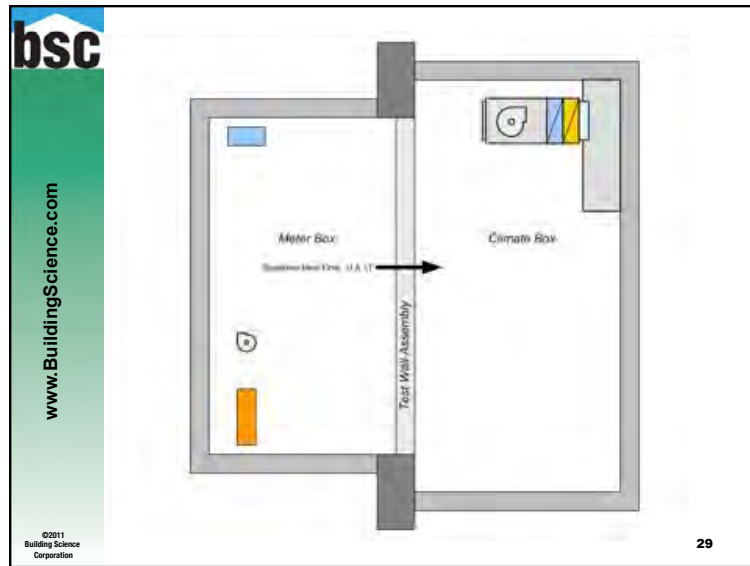
- A Controlled, repeatable conditions
- Measure heat & mass flows



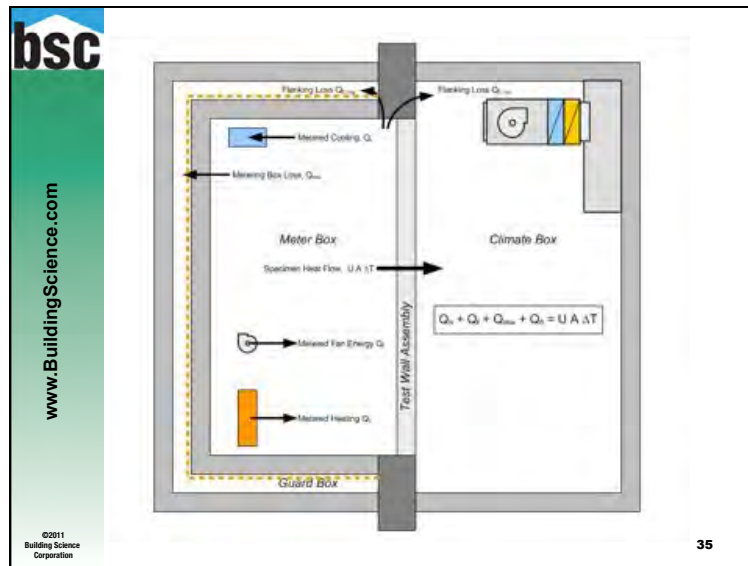
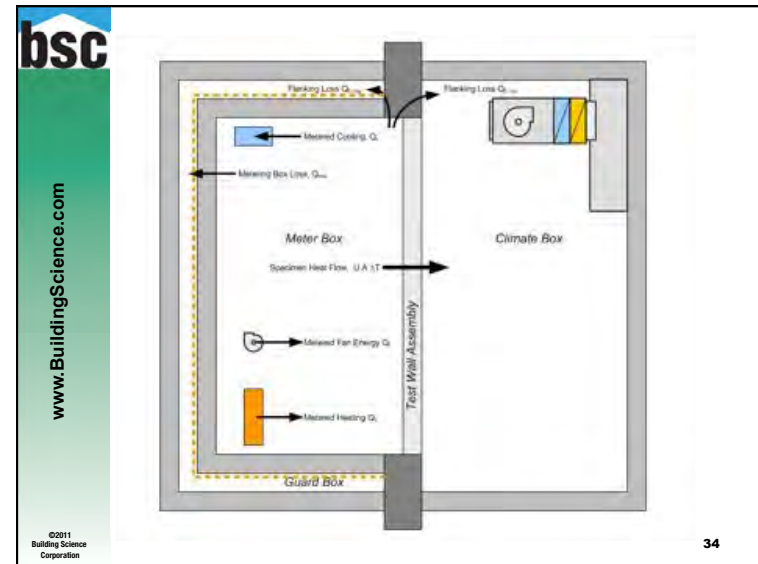
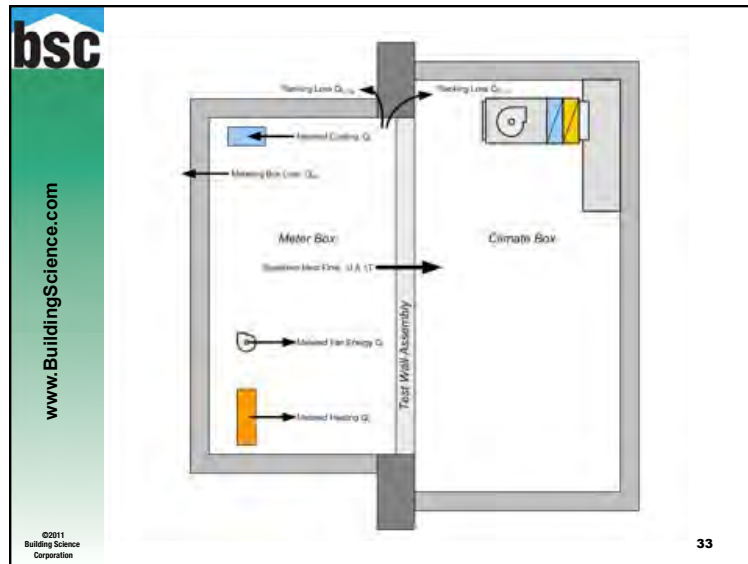
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## Hot Box

- ❑ Double Guard
- ❑ Deep Meter Box
  - ❑ accommodate complex geometries
  - ❑ e.g. wall / floor intersections
- ❑ Meter Box heating & cooling
- ❑ Measure energy and mass flows
  - ❑ Air transfer system
  - ❑ Tracer gas system

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## Hot Box

- ❑ Wall specimen size:  
8' x 12' (2.4 x 3.6 m)
- ❑ Temperature range:  
-40 to 150 F (-40 to 65 C)
- ❑ deltaP & air flow:  
+/-75 Pa & 30 cfm (300 lpm)

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## Method

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## Three Key Elements:

- ❑ Wall specimen 'blanks'
  - ❑ Wall frames with controlled, realistic & reproducible airflow paths
- ❑ Testing with imposed pressure difference
  - ❑ 10 Pa driving Exfiltration & Infiltration
- ❑ Measurement of the air movement
  - ❑ Tracer gas for ALL tests

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## Wall specimen 'blanks'

- ❑ Framed walls designed and constructed to allow airflow paths that are
  - ❑ Realistic
  - ❑ Controlled
  - ❑ Reproducible

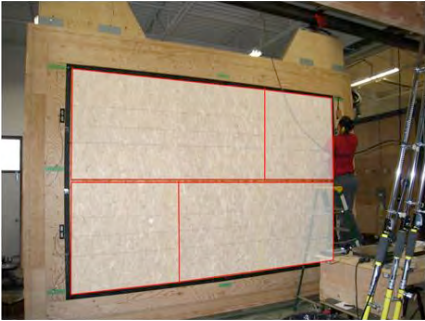
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### Airflow path 1 of 3

- 1/8 in. horizontal gap between sheathing (per APA installation recommendations)



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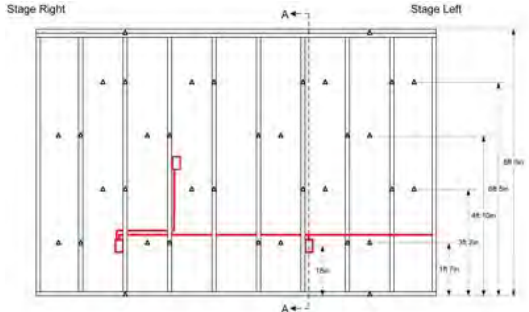
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### Airflow path 2 of 3

- 3 standard (non-gasketed) electrical boxes and associated wiring (precedence Ober 1994, NAHB 2009)



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### Airflow path 3 of 3

- 1/32 in. gaps between top & bottom plates and OSB & GWB
- Controlled* – use high tolerance steel shims
- Realistic* – representative of gaps that open as framing dries & shrinks (Onysko & Jones, 1989)
- Reproducible* – air leakage for the same wall four constructed times:  
0.22 to 0.26 cfm50/ft<sup>2</sup>

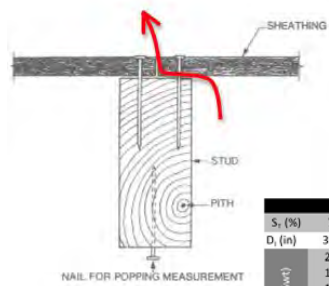
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### Onysko & Jones



$$\Delta D = \frac{D_1(M_2 - M_1)}{30(100)/S_T - 30 + M_1} \quad (13-3)$$

Ending MC (%wt)	Predicted change in dimension (in/1000)						
	S <sub>r</sub> (%)	7	18	16	14	12	10
D, (in)	3.5	20	18	16	14	12	10
	20	0	17	34	51	68	86
	18	-17	0	17	34	51	69
	16	-33	-17	0	17	34	51
	14	-50	-34	-17	0	17	34
	12	-67	-50	-34	-17	0	17
	10	-84	-67	-51	-34	-17	0
	8	-100	-84	-68	-51	-34	-17
	6	-117	-101	-84	-68	-51	-34

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## Onysko & Jones

- At 10 Pa pressure difference shrinkage resulted in 4x increase in air leakage

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## Shims

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**SPACE**  
Kitchener, Ontario

ARBOR SHIM WITHOUT KEYWAY  
3/4" ID X 1-1/8" OD X .031" THK  
STEEL AISI 1010 PLAIN

1 PK / 10 EA

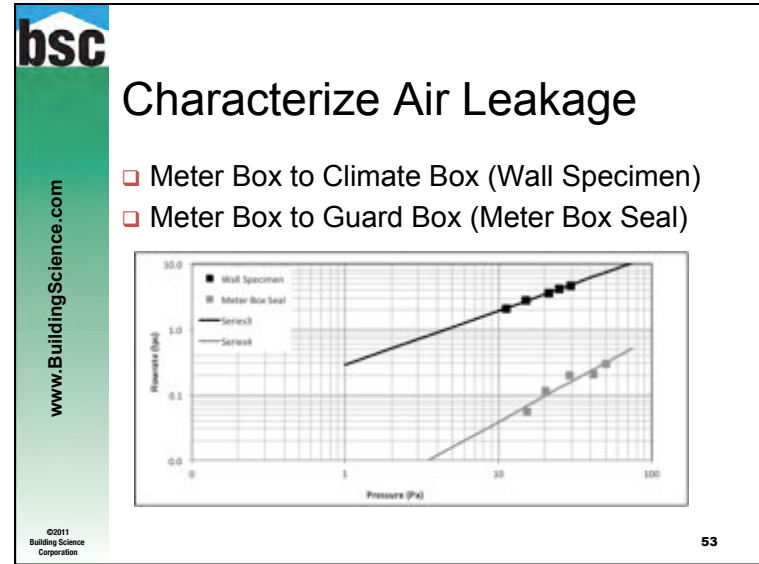
Use By

Lot

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## Realistic boundary conditions

Test Segment	1	2	3	4	5	6	7	8	9
MB	72	72	72	72	72	72	72	72	72
CB	-18	0	0	0	33	108	108	108	144
ATS			Infil	Exfil			Infil	Exfil	

- 9 Test Segments:
  - 5 without intentionally induced airflow
  - 4 with intentionally induced airflow
- But what air pressure difference should be used to induce the airflow?

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## Air Pressures Differences

- Weather station wind pressures typically 8-13 Pa
- House wind pressures typically 3-5 Pa

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## Air Pressure Differences

- Stack effect pressures typically 1-2 Pa /floor

Tout		Stack
C	F	Pa
30	86	-0.95
10	50	1.24
0	32	2.45
-10	14	3.75
-20	-4	5.16

\*Stack effect pressures for a 2 storey house

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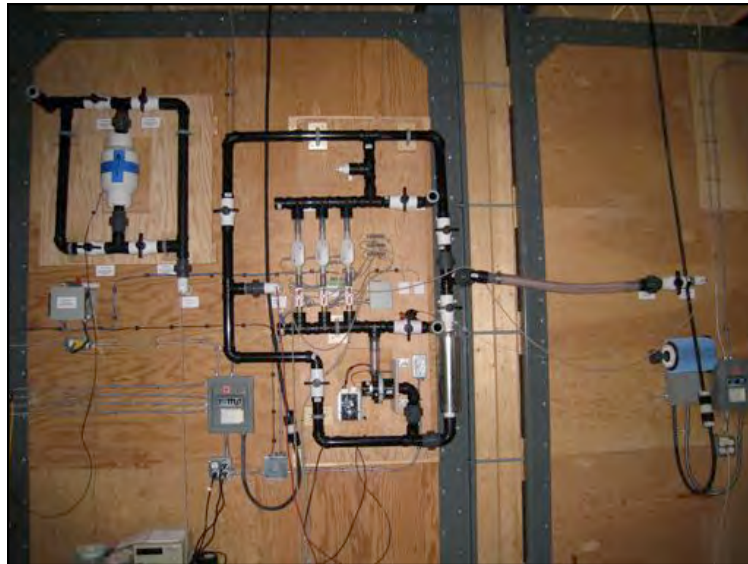
## Air Pressure Differences

- Wind pressure: 3-5 Pa
- Stack effect: 1-2 Pa
- Fan pressures: ? but assume negligible
- Test air pressure of 10 Pa is reasonable and repeatable

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## Challenges testing *real* walls

- ❑ Realistic wall with airflow paths
- ❑ Generate realistic temperature conditions
- ❑ Induce realistic pressure differences
- ❑ Measure heat & mass

- ❑ But... airflow can occur in hot boxes even when we don't *intentionally* induce it

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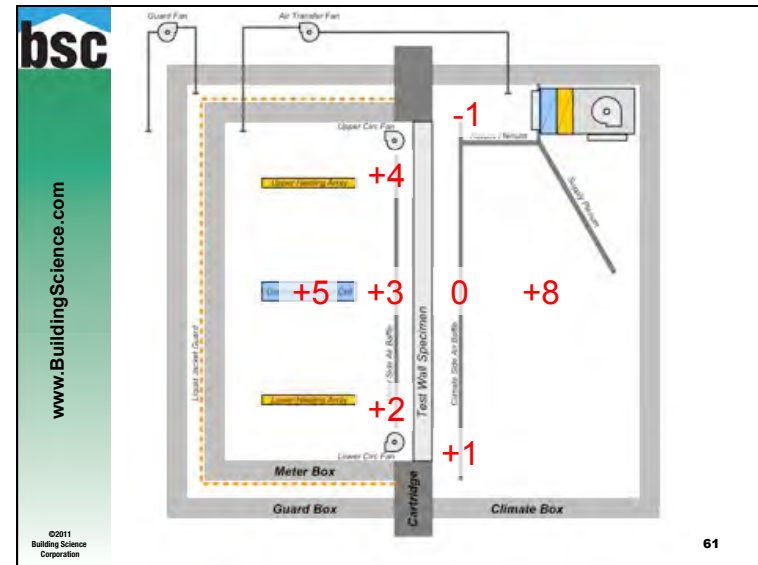
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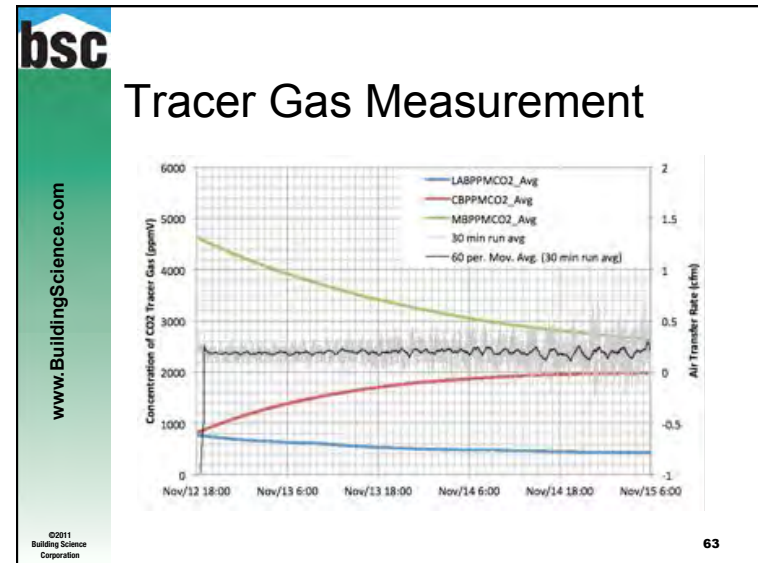
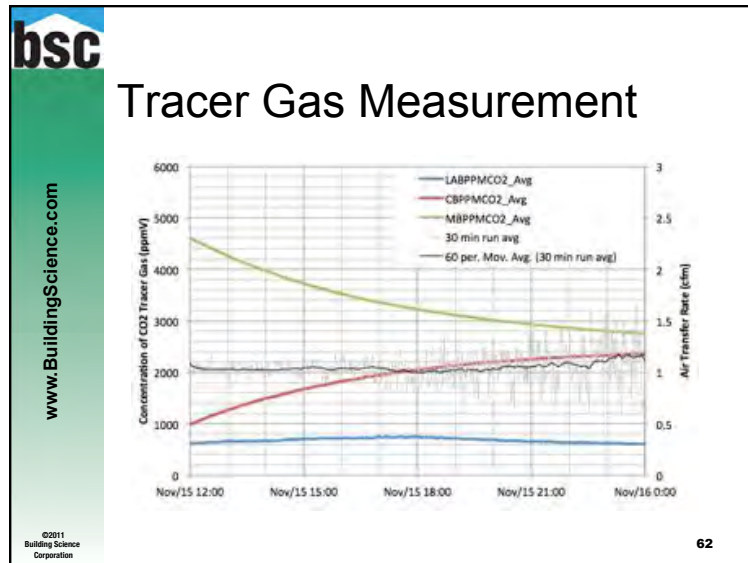
## Unintended Pressures

- ❑ Air pressure differences exist even when we don't intentionally induce them
- ❑ Typically between 0.5-3 Pa
- ❑ Can have a significant impact on 'leaky' walls

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**Can impact of air leakage be assessed?**

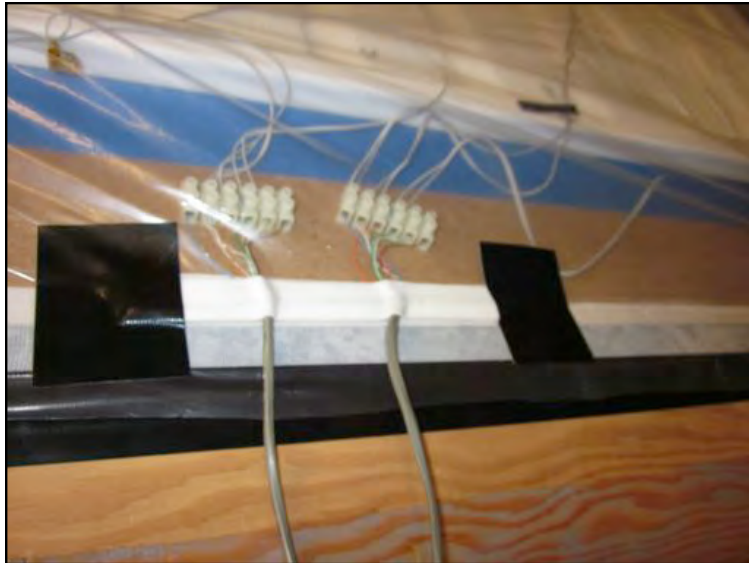
- ❑ Not easily!
- ❑ We can't assess the impact of the airflow (i.e. the interaction effect) unless we know how a perfectly airtight wall performs (i.e. when there is no airflow through it)
- ❑ So... test the wall again with ***inside and outside sealed.***

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## 'Sealed' wall test conditions

- Again start by characterizing leakage
- Test 5 temperature differences

Test Segment	1	2	3	4	5
MB	72	72	72	72	72
CB	-18	0	33	108	144
ATS					

- No intentionally induced airflow
- Tracer gas measurement of air change

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## Thermal Metric Test Method

1. Construct wall frame
2. Complete construction of wall specimen
3. Test 'air leaky' wall thermal performance
  - a) Characterize leakage (PvsQ)
  - b) 5 climate temps w/ NO\* imposed deltaP
  - c) 2 climate temps w/ +ve & -ve 10 Pa deltaP
4. Seal the wall specimen (inside & out)
5. Test 'sealed' wall thermal performance
  - a) Characterize leakage (PvsQ)
  - b) 5 climate temps w/ NO\* imposed deltaP

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## Some Test Results

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### A proof of concept wall

- ❑ Wall comparison: (Leaky) vs (Tight)
- ❑ GWB
- ❑ 2x4 w/ air permeable insulation
- ❑ 1.5" air impermeable exterior insulation
- ❑ Vinyl Siding
- ❑ NONE of the products produced by the TM industry partners

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### Lessons

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## Lesson 1: Material R-values

- ❑ Temperature effects R-value
- ❑ Density effects R-value
- ❑ Moisture content effects R-value

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## Lesson 2: Assembly R-value

- ❑ Hand Calculations (parallel path)
  - ❑ Works if
    - materials have similar R-value (e.g. wood frame wall)
  - ❑ Does not work if
    - materials have very different R-value
    - highly conductive layers perpendicular to flow
- ❑ Computer Simulations (Therm, Heat2, etc.)
  - ❑ Works if there is NO air movement

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## Lesson 3: Hot Box Testing

- ❑ Airflow impacts common hot box tests!
- ❑ Tracer gas can be used to measure incidental airflows

Description	SI Units *		British Units	
Specimen Area	5.946	m <sup>2</sup>	64.00	ft <sup>2</sup>
Specimen thickness	153.00	mm.	6.024	in.
Average cold side surface temperature	-22.91	°C	-9.24	°F
Average warm side surface temperature	15.66	°C	60.20	°F
Temperature differential	38.57	°C	69.43	°F
Mean specimen temperature	-3.62	°C	25.48	°F
Rate of heat flux through the specimen	43.126	W/m <sup>2</sup>	13.670	Btu/h.ft <sup>2</sup>
Thermal conductance of the specimen	<b>1.118</b>	W/m <sup>2</sup> .K	<b>0.197</b>	Btu/h.ft <sup>2</sup> .°F
Thermal resistance of the specimen	<b>0.894</b>	K.m <sup>2</sup> /W	<b>5.079</b>	°F.ft <sup>2</sup> .h/Btu
Thermal conductivity of the specimen	0.171	W/m.K	1.186	Btu.in./h.ft <sup>2</sup> .°F
Thermal resistivity of the specimen	5.846	K.m/W	0.843	°F.ft <sup>2</sup> .h/Btu.in.
Uniform Baffle Air Velocity (Warm Side)	0.22	m/s	0.98	ft/sec
Uniform Air Velocity (Cold Side)	3.0	m/s	9.84	ft/sec
Pressure Differential Across Specimen	Nil	Pa	Nil	psi
Warm Side Chamber Relative Humidity	10.1	% RH	10.1	% RH
Steady-State Temperature Differential Between Guard & Metering Chamber	-0.02	°C	-0.036	°F

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