Thermal Energy Storage in High Performance Buildings



Photo credit Bruce Coldham



Photo credit Hillside

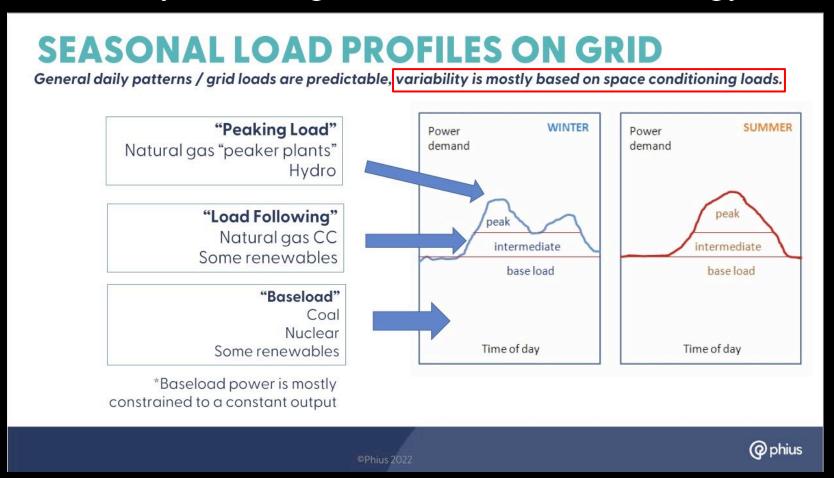


Photo credit Amanda Nickerson

Twenty-Sixth Westford Symposium on Building Science

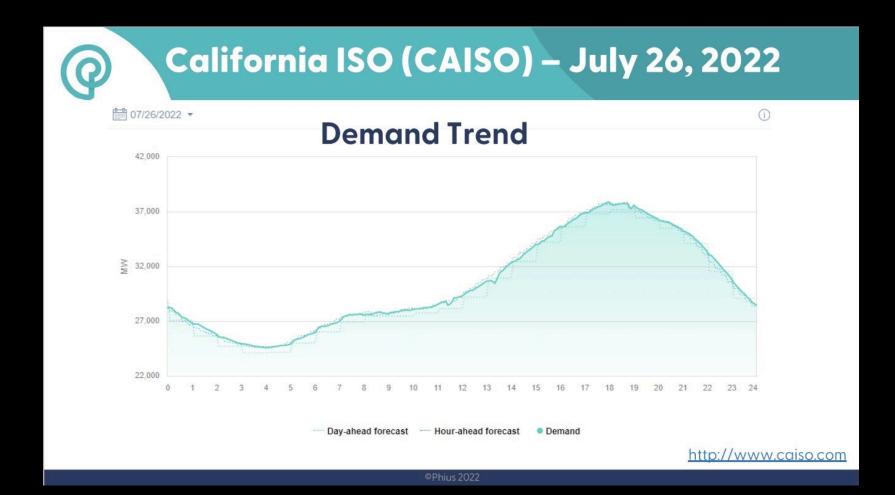
Why Bother?

Grid Stability and Integration of Renewable Energy Sources

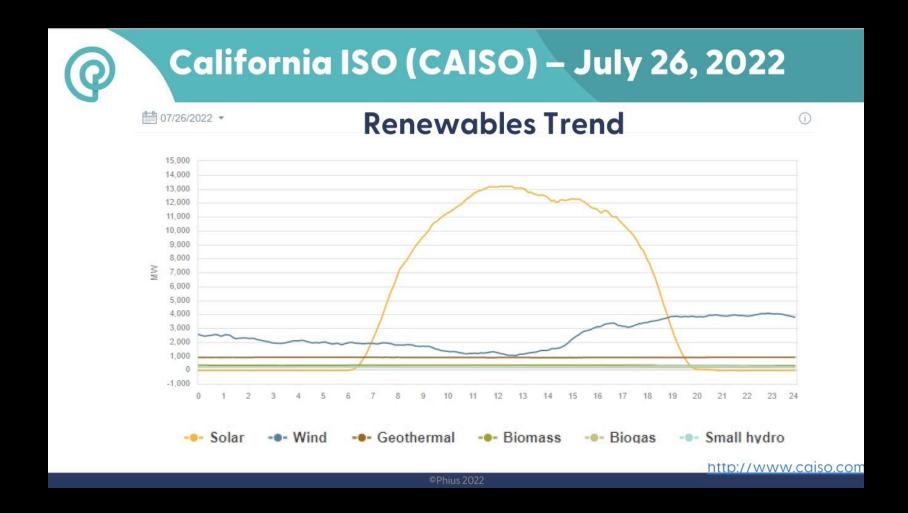


Huge Thanks to Lisa White and PHIUS for these slides

CA ISO Load



CA ISO Renewable Generation



CA ISO Load After Renewables



11 GW in 3 hours! (MA PV capacity ~3 GW)

ISO-NE

New England ISO – April 2, 2022



Emissions Vary

Not all kWh's (used and produced) are equal

Hourly Marginal
Carbon
Emissions will
continue to be
dynamic.

Price to meet peak grid loads will remain dynamic.



Source: WattTime CHICAGO, IL - 2019

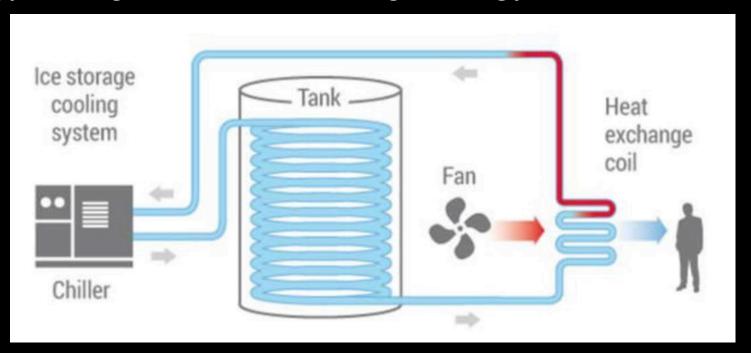


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Strategies

- Load reduction in buildings, both thermal and electrical
- Grid-interactive control two way grid
- Load shifting in time

Energy storage is a load-shifting strategy



Why Bother?

Solar Net Metering Is Under Threat All Over The US

NET METERING UNDER ATTACK (AGAIN)!

February 21, 2023 | 2 min read

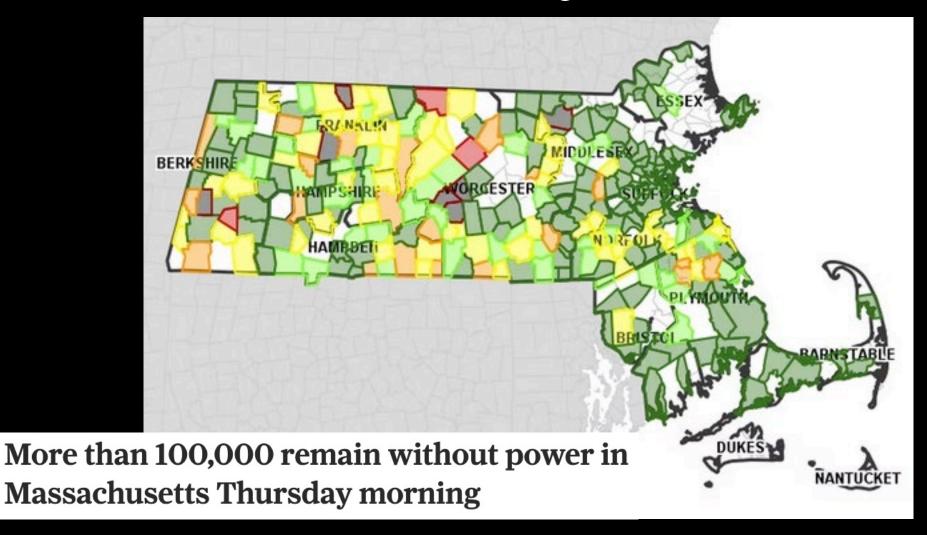
Solar energy under attack in Florida

Juest Post: Why Is Net Metering Under Attack?

The utilities' net metering math doesn't add up.

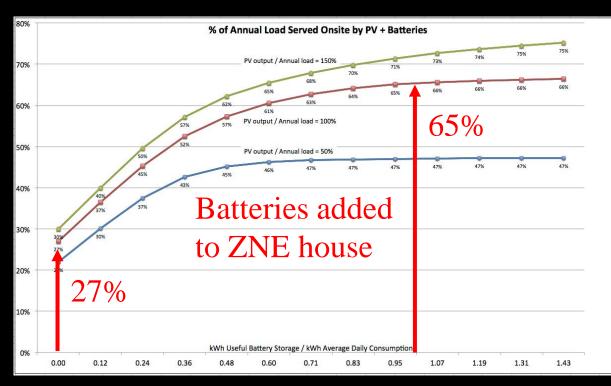
Why Bother?

Resilience in Grid Outage Events



Electric Storage Batteries

- Most flexible type of storage
- Provides grid outage resilience
- Provides load shifting and peak shaving
- Boosts % of site-generated energy that is consumed on-site





Electric Storage Batteries

- Expensive
- Capacity drops over time
- Don't provide the inherent resilience of a superb enclosure with thermal storage
- Best application may be in distributed microgrids
- For many of us as homeowners, V2B is the future

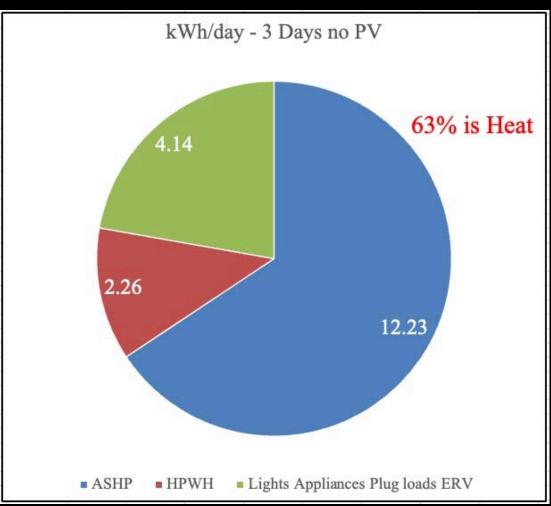




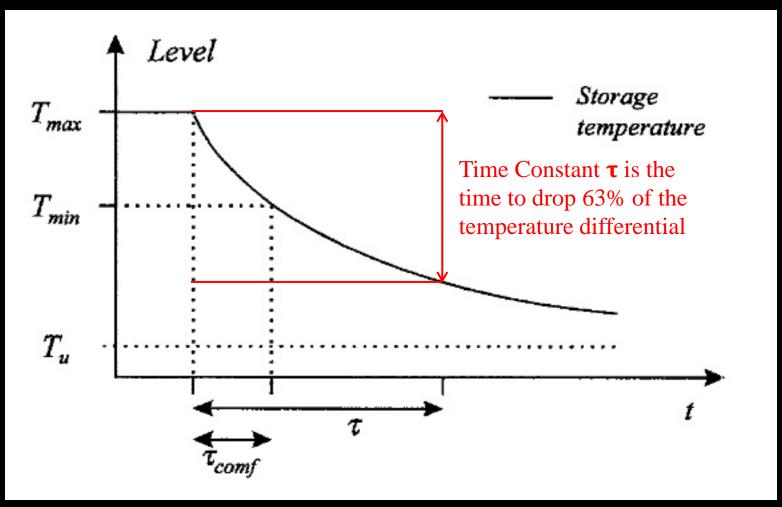
Heat is the Biggest Load

Electric usage
February 8th-10th 2016
after snowstorm
covered the PV system.
Superinsulated house
with passive solar gain





Time Constant



From On the thermal inertia and time constant of single family houses, Hedbrant

Time Constant for Buildings

Thermal Capacity per °F change in temperature (BTU/°F)

Heat loss coefficient, UA (BTU/hr-°F)

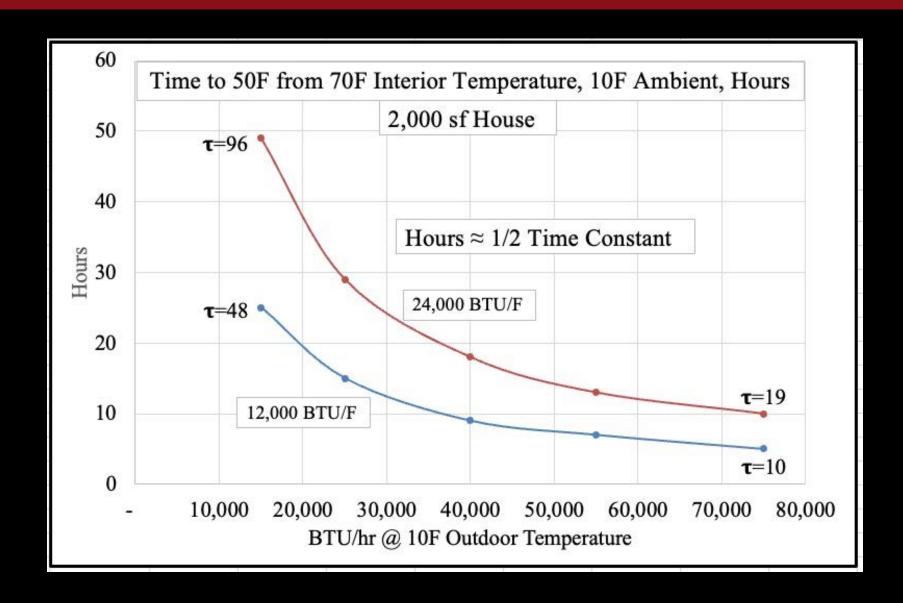
A range of thermal capacity of light frame houses might be 5-7 BTU/sf-°F

A range of UA of light frame houses might be 0.125 – 0.625 BTU/hr-sf-°F (2000 sf house 15-75,000 BTU/hr)

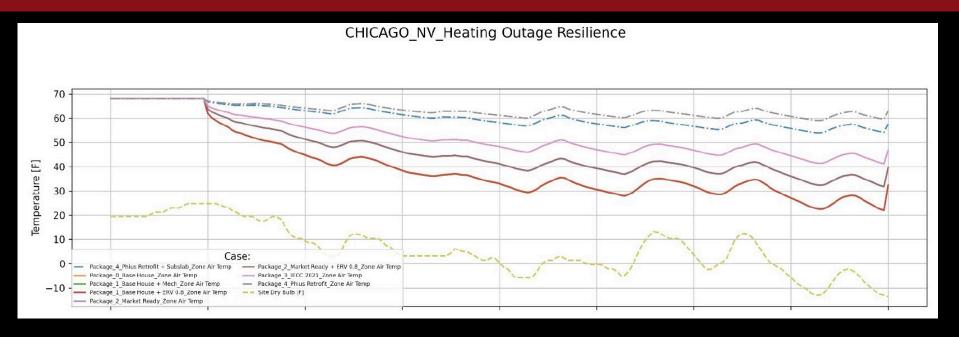
Therefore, a range of time constant of light frame houses would be 10-50 hours

A 2018 paper (John et al) analyzed data from over 10,000 Ecobee thermostats and estimated that a majority of time constants were in the 15-55 hour range

Time Constant and Cool Down

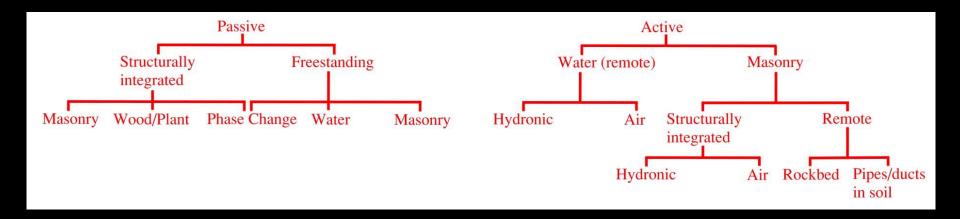


1 Week Heating Resilience

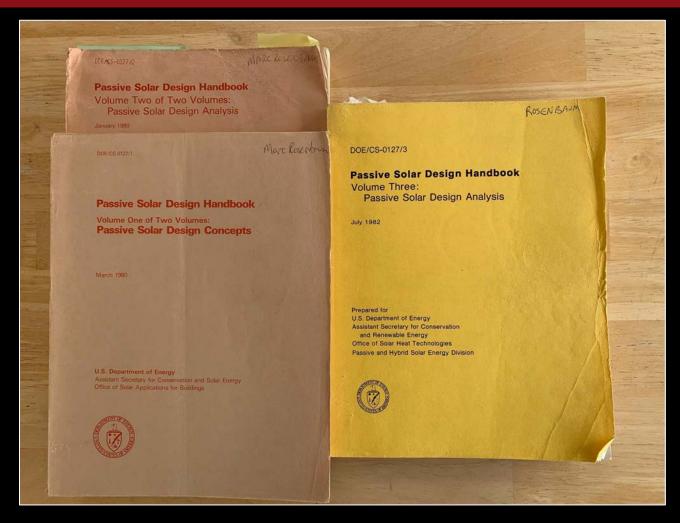


Thanks to Al Mitchell, Graham Wright, and PHIUS for this slide

A Taxonomy of Thermal Storage



Passive Solar Design Handbooks



https://www.osti.gov/servlets/purl/5672634

Passive Freestanding

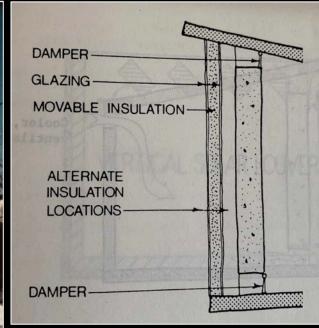




Photos courtesy of Amanda Nickerson and E. Lord – Society for the Protection of New Hampshire Forests Conservation Center – Banwell Architects

Passive Structurally Integrated





Doug Kelbaugh's Trombe (mass) wall house in Princeton NJ 15" concrete with black selective surface
Mass walls delay the solar heat delivery (best when unvented)

Passive Thermal Storage

The material parameter that matters is thermal effusivity e

$$e = \sqrt{k*\rho*Cp}$$

Thermal effusivity is a measure of a material's ability to exchange thermal energy with its environment.

The square root of thermal conductivity (k) times density (ρ) times specific heat (Cp). Density times specific heat is volumetric heat capacity - how much heat a material holds per degree of temperature change (BTU/ft³-°F).

So, how much energy can penetrate into the surface of a material is dependent on both how well it conducts heat, and how much heat it can hold.

Thermal Effusivity of Materials

Material	Density, lb/ft3	Conductivity, BTU/hr-ft-°F	Specific heat, BTU/lb-°F	Heat capacity, BTU/ft3-°F	Thermal effusivity, BTU/ft-°F-√hr
Cast iron	450	28	0.12	54	38.9
Concrete	150	1.16	0.19	28	5.69
Gypsum plaster	81	0.29	0.26	21	2.47
Softwood	27	0.067	0.76	20	1.17
Drywall	50	0.093	0.26	13	1.1
Fiberglass batt	0.8	0.025	0.16	0.12	0.06

Thin layers of materials like plaster and wood can store usable amounts of heat when applied over lots of area

Direct Gain Passive Guidelines

- Up to 7-8% net S glazing/floor area needs no additional storage
- Above that, 5-6 sf of directly sunlit thermal storage per 1 sf additional sf of glazing
- Or, 40 sf of indirect (convective) thermal mass connected to the space (here, thin is OK)

Plaster and wood



Straw Bale and Timber - New Frameworks Natural Building

Masonry floors, wood structure & decking



Kern Center Living Building Hampshire College – Bruner Cott

Masonry floors, wood structure & decking



Winston Underground House – Don Metz Architect

Cross-laminated Timber







Precast Concrete (or other masonry?)





Hillside Center for Sustainable Living
Hall & Moskow (developers) Moskow Linn Architects



Middlebury Bicentennial Hall – Payette Architects

Precast Concrete



- Precast concrete on steel beams
- Absorbs daily heat (no A/C)
- Shape reflects uplighting down
- Shape reflects sound onto sound absorption panels

Wessex Water – Bath, England Bennetts Architects Buro Happold Engineers

Integration of design team from

conceptual stage

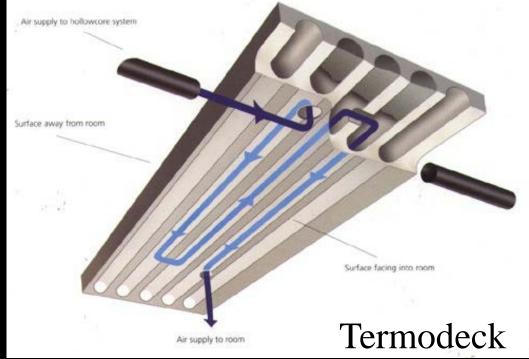


Active Thermal Storage

- Storage is (usually) remote
- Storage is dispatchable according to need
- Much higher ΔT is possible
- Power is needed to charge/discharge (not always both)

Masonry Structurally Integrated - Air



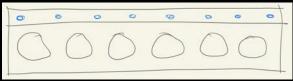




- Hollowcore precast planks
- Ventilation air delivered in space conditioning air
- 35,000 sf building, 5 zones
- CMU walls add passive mass
- Highest occupant satisfaction in PROBE Study

Masonry Structurally Integrated - Hydronic





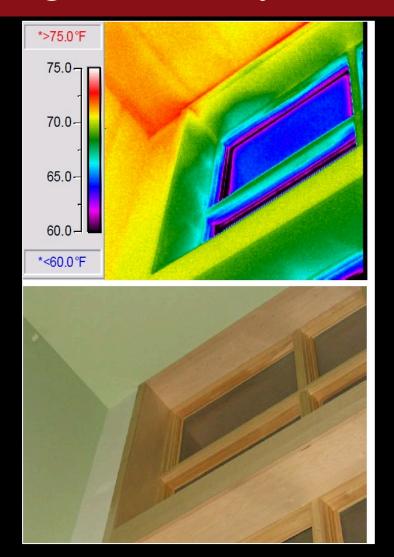


- PEX tubing in topping slab over precast hollowcore plank
- Both floor and ceilings are thermally active
- Floor dominates in heating; ceilings dominate in cooling
- Latent load removed in ventilation air

Dartmouth McLaughlin Dorms – Moore Rubell Yudell / Bruner Cott Dan Nall – mechanical engineer

Masonry Structurally Integrated - Hydronic





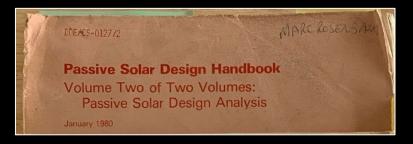
PEX tubing in topping slab over precast hollowcore plank

Fan-forced Rockbed

Active storage; passive release



Solar attic above greenhouse charges the air up to 110°F for more energy stored per CFM in this VT house

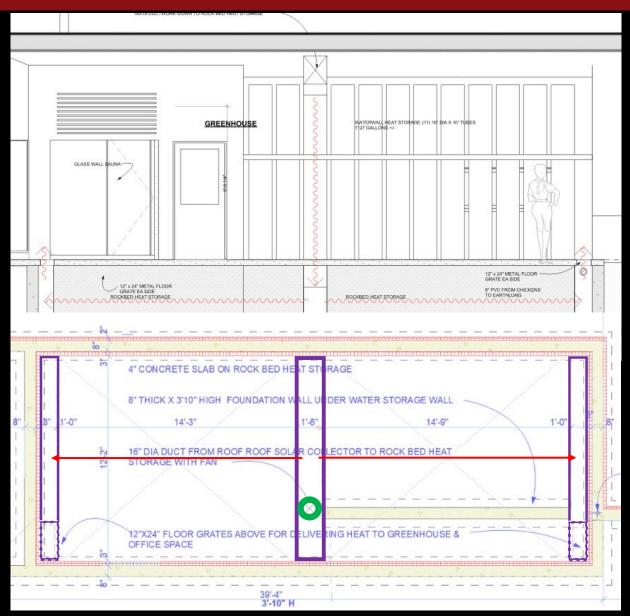




Natick Community Greenhouse – Jon Romig Architect

Marc Rosenbaum, PE – Energysmiths – West Tisbury, MA

Fan-forced Rockbed

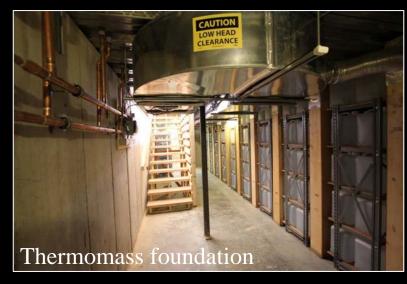


Fan-forced Water Containers

Active storage; passive release







45°F min. temp. at -7°F outdoors



 $Marc\ Rosenbaum,\ PE-Energy smiths-West\ Tisbury,\ MA$

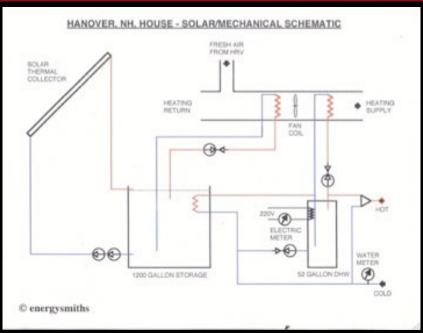
Fan-forced Water Containers

Active storage; passive release

Q, CFM	70	Q, ft3/sec	1.17	ΔP, psi	0.0071
g, ft/sec2	32.2			ΔP, inches of water	0.197
D, inch	0.25	D, ft	0.0208	ΔP, Pascals	50
rho, lb/ft3	0.075			V, ft/min	1245
Cd	0.70			V, ft/sec	20.7
Number of holes	165	A, ft2	0.056	3	3



Active Solar Thermal Water Storage









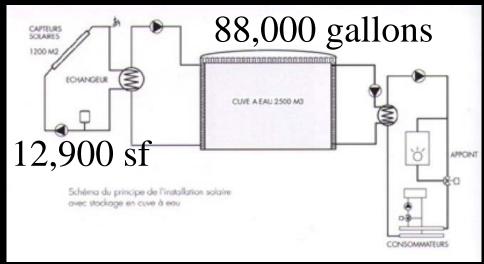
Back-up energy in very low energy solar buildings varies year to year (2:1 here)

1,200 gallons @ 80°F ΔT = 800,000 BTU

Active Annual Solar Thermal Water Storage



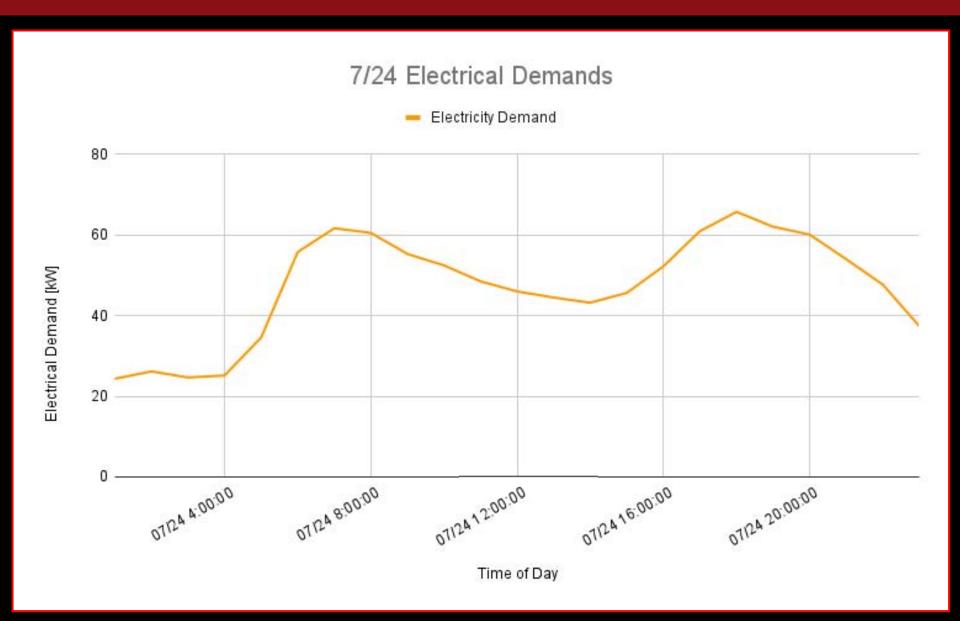
Swiss Federal Statistics Building

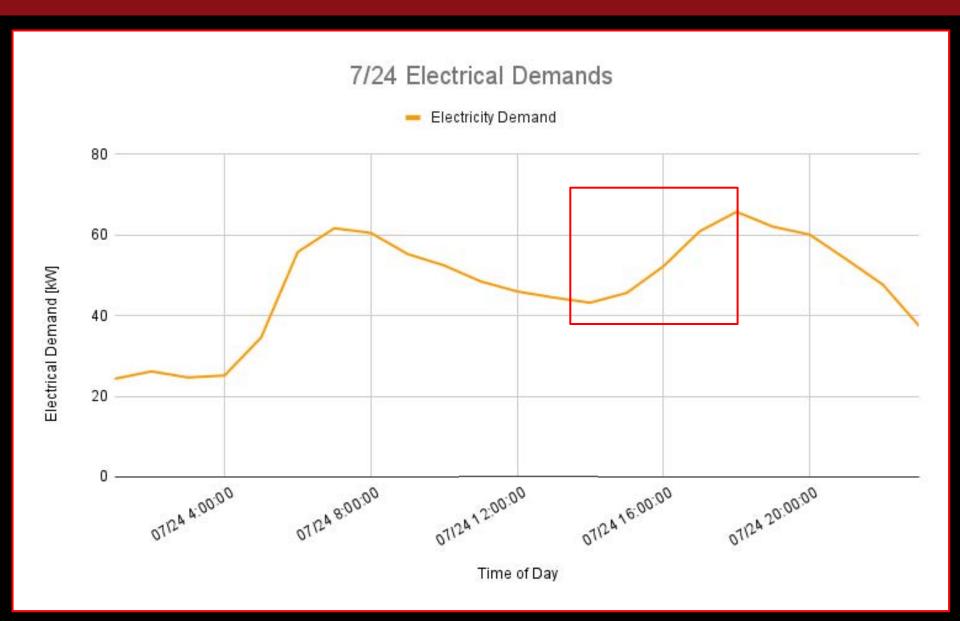


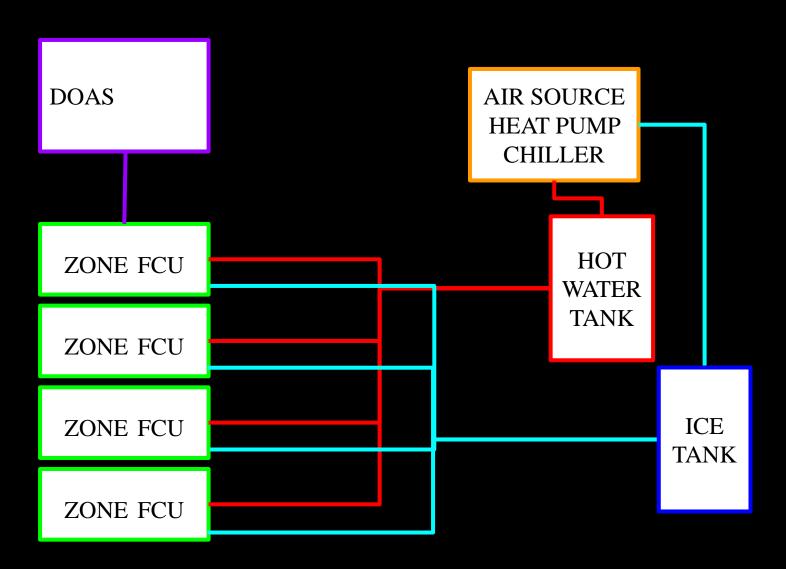
- Prototypical Multifamily
- 23,300 sf
- 32 Units
- Phius Enclosure Spec

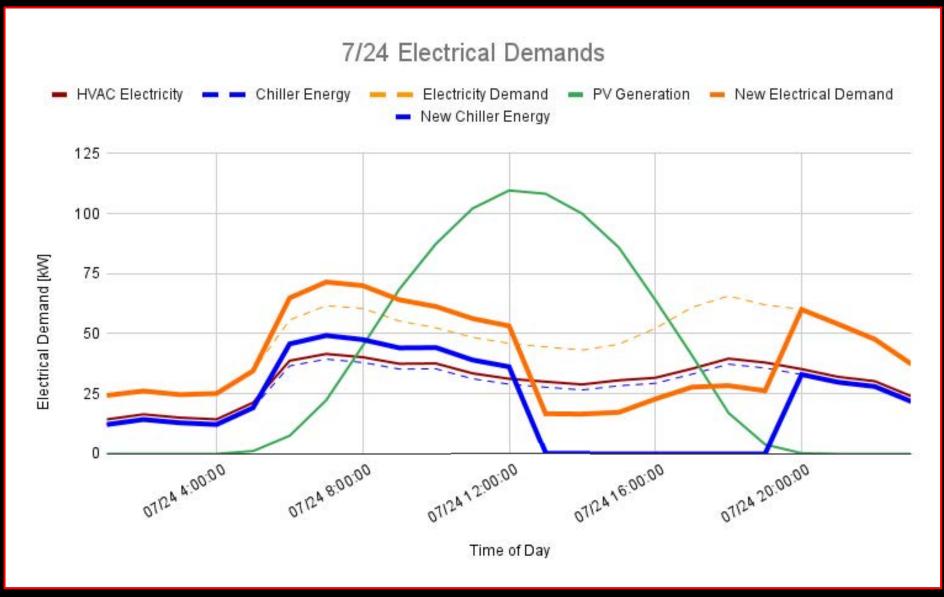


Thanks to Al Mitchell and PHIUS for these slides









PV/A-WHP w/ Thermal Water Storage

- 4,500 sf footprint airplane hangar with office space
- Owner wanted maximum onsite consumption of solar energy
- Non-optimal solar orientation and tilt
- A-WHP and hydronic radiant floor slab
- "Brick in a box" Excel hourly model to inform sizing of storage and PV
- Hourly model of PV gain and outdoor temp from PV Watts
- Hourly heating; cooling; DHW; EV; plug and lighting loads
- A-WHP COP vs. outdoor temp varied from manufacturer's data

UA, BTU/hr/F	1,007	Setpoint, F	68			
Month	Day	Hour	Ambient Temp, F	Heat loss, BTU/hr	Heat pump COP	Heat pump usage, kWh
1	1	0	28.4	39,865	3.0	3.9
1	1	1	28.4	39,865	3.0	3.9
1	1	2	28.4	39,865	3.0	3.9
1	1	3	26.6	41,677	3.0	4.1
1	1	4	26.6	41,677	3.0	4.1
1	1	5	26.6	41,677	3.0	4.1
1	1	6	26.6	41,677	3.0	4.1
					9	

Model Inputs and Outputs

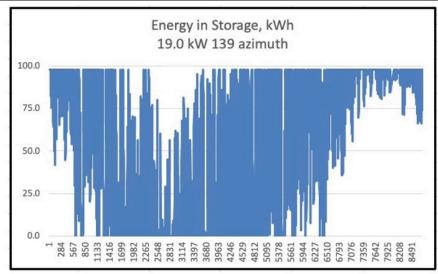
Thermal storage capacity, kWH 98							Thermal storage capacity, gallons H2O						100	00			Stora	ge temp	high li	mit	125
										67	=					Storage temp			low lin	mit	85
				100		-								Do	of ana	PV W		0 1	1		
1														Ko		2000	170000				
11	P	V array	139,	kW	19.	0									1055		18 N	Max roof a	rea at 8	0% = 18	324 sf
	Ъ	V array	310	ιw	0.	0									0		18		1		
		v array	517,	K VV	v.	U	-		-						U		10				
		PV generated, kWh	DHW, kWh	Cooling,	P/L/A, kWh	EV, kWh	Heating, kWh			Total non- heating used, kWh	Grid energy imported serving non- heating, kWh	Total load, kWh	use served directly by PV,	Heating loads served directly by PV, kWh	Grid energy into heating, kWh	Total imported grid energy, kWh	PV energy into thermal storage, kWh	PV energy exported, kWh	PV generation/ load	Fraction of PV energy used on site	
		22925	702	702	6302	2118	13107			9824	5204	22931	4620	3280	5241	10445	438	10644	100%	54%	
Ī	Max	15.0	0.1	0.5	5 1.3	1.7	5.7			2.7	13.8	14.9	4.6	14.9	12.7	14.9	5	5.7 10.7	51.1	13.0	
	Total	22925	702	702	2 6302	2118	13107			9824	18305	47237	3280	35032	17239	17793	524	41 4381	17237	10644	
Date/Time		PV, kWh	DHW, kWh	Cooling,	P/L/A, kWh	EV, kWh	Heating,			Use except heating, kWh	Control of the Contro	Heating	heating	Remaining heating	Heat extracted from storage,	Remaining heat load,	Grid energy in heating,	thermal	Energy added to storage,	Surplus PV exported to the grid,	Energy in Thermal Storage,
9/1/2014 0:00		PV, KWII	DHW, KWN		P/L/A, KWn	EV, KWH				KWI											
		0.0	0.06	0.09	0.35	0.00		0.00	0.00	0.5		load, kWh		load, kWh	kWh	kWh	kWh 0	storage, kWh	kWh	kWh	kWh 97.7
9/1/2014 1:00		0.0 0.0	0.06 0.06			0.00	0.00	0.00	0.00		0.0		0.0	0.0 0.0		0.0	0		0.0	0.0	
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9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 8:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6	0.06 0.06 0.06 0.06 0.12 0.12 0.12	0.20 0.20 0.14 0.09 0.09 0.09 0.09 0.09	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 0.88	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.6 0.6 0.5 0.5 0.6 0.7 1.1 1.1 1.1	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8	3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	000000000000000000000000000000000000000	0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 8:00 9/1/2014 9:00 9/1/2014 1:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9	0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.12	0.2(0.2(0.14 0.09 0.09 0.09 0.09 0.09 0.09	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.53 9 0.88 9 0.88 9 0.88 9 1.23 4 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6 0.5 0.5 0.6 0.7 1.1 1.1 1.1 1.4	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4	3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	000000000000000000000000000000000000000	0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 10:00 9/1/2014 10:00 9/1/2014 11:00 9/1/2014 13:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6	0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.12 0.06 0.06 0.06	0.20 0.20 0.14 0.05 0.06 0.09 0.09 0.09 0.09 0.09 0.14 0.14	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 0.88 9 1.23 4 1.23 4 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.6 0.5 0.5 0.5 0.6 0.7 1.1 1.1 1.1 1.4 1.4	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5	3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 6:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 1:00 9/1/2014 11:00 9/1/2014 11:00 9/1/2014 12:00 9/1/2014 13:00 9/1/2014 13:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0	0.06 0.06 0.06 0.12 0.12 0.12 0.06 0.06 0.06 0.06	0.20 0.20 0.14 0.09 0.09 0.09 0.09 0.09 0.14 0.14 0.15	0 0.35 0 0.35 4 0.35 9 0.35 9 0.53 9 0.53 9 0.88 9 0.88 9 0.88 9 1.23 4 1.23 4 1.23 9 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.6 0.5 0.5 0.5 0.6 0.7 1.1 1.1 1.4 1.4 1.4 1.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5 4.6	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5 4.6	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 7:00 9/1/2014 8:00 9/1/2014 9:00 9/1/2014 11:00 9/1/2014 11:00 9/1/2014 11:00 9/1/2014 11:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 15.4	0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.12 0.06 0.06 0.06 0.06 0.06 0.06	0.20 0.21 0.01 0.09 0.09 0.09 0.09 0.09 0.14 0.12	0 0.35 0 0.35 1 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 0.88 9 1.23 4 1.23 9 1.23 9 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.5 0.5 0.5 0.6 0.7 1.1 1.1 1.1 1.4 1.4 1.5 1.5	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5 4.6 4.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 9.8 10.4 10.9 6.2 6.5 4.66	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 1:00 9/1/2014 10:00 9/1/2014 11:00 9/1/2014 13:00 9/1/2014 13:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 5.4	0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.10 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.20 0.20 0.14 0.09 0.09 0.09 0.09 0.09 0.09 0.14 0.15 0.15	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.53 9 0.88 9 0.88 9 1.23 4 1.23 9 1.23 9 1.23 9 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.66 0.5.0 0.5.0 0.6.6 0.7.1 1.1 1.1 1.4 1.4 1.5 1.5 1.5 1.5 1.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 19.8 10.4 10.9 6.2 6.5 4.6	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 10.4 10.9 6.2 6.5 4.6	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 7:00 9/1/2014 7:00 9/1/2014 9:00 9/1/2014 1:00 9/1/2014 1:00 9/1/2014 1:00 9/1/2014 1:00 9/1/2014 1:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 15.4	0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.12 0.06 0.06 0.06 0.06 0.06 0.06	0.20 0.21 0.01 0.00 0.00 0.00 0.00 0.00	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.53 9 0.88 9 0.88 9 1.23 4 1.23 4 1.23 9 1.23 9 1.23 9 1.23 9 0.88	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6.0.5 0.5.5 0.6.6 0.7.7 1.1 1.1.1 1.4.4 1.4.5 1.5.5 1.5.5 1.5.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 10.4 10.9 6.2 6.5 4.6 4.0 0.9 9	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 1:00 9/1/2014 11:00 9/1/2014 12:00 9/1/2014 13:00 9/1/2014 14:00 9/1/2014 15:00 9/1/2014 16:00 9/1/2014 16:00 9/1/2014 17:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 5.4 2.4	0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.02 0.06 0.06 0.06 0.06 0.06 0.06 0.0	0.20 0.21 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0	0 0.35 0 0.35 14 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 0.88 9 1.23 4 1.23 4 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.6 0.7 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5.5 8.1 10.4 10.9 6.2 6.5 5.5 6.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 9:00 9/1/2014 10:00 9/1/2014 11:00 9/1/2014 13:00 9/1/2014 14:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 17:00 9/1/2014 17:00 9/1/2014 17:00 9/1/2014 17:00 9/1/2014 19:00 9/1/2014 19:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 5.4 2.4 0.5 0.0	0.06 0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.0	0.20 0.21 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.11 0.11 0.11 0.12 0.22 0.23 0.33	0 0.35 0 0.35 4 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 1.23 4 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 7 0.88	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6 0.5 0.5 0.5 0.6 0.7 1.1 1.1 1.1 1.4 1.4 1.5 1.5 1.5 1.5 1.3 1.3 2.2 2.6	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5 8.1 10.4 10.9 6.2 6.5 6.5 4.6 4.0 0.9 9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 5:00 9/1/2014 6:00 9/1/2014 8:00 9/1/2014 1:00 9/1/2014 11:00 9/1/2014 11:00 9/1/2014 12:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 18:00 9/1/2014 18:00 9/1/2014 18:00 9/1/2014 19:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 5.4 2.4 4.0.5 0.0 0.0	0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.12 0.16 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.20 0.2(1) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0 0.35 0 0.35 1 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 1.23 1 1.23 9 1.23 9 1.23 9 1.23 8 0.88 9 8.88 7 0.53 7 0.55 7 0.35	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.5 0.6 0.7 0.7 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5.5 8.1.1 9.8 10.9 6.2 6.5 4.6 4.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5,5 8.1 10.4 10.9 6.2 6.5 4.6 4.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7
9/1/2014 1:00 9/1/2014 2:00 9/1/2014 3:00 9/1/2014 4:00 9/1/2014 6:00 9/1/2014 7:00 9/1/2014 10:00 9/1/2014 10:00 9/1/2014 11:00 9/1/2014 13:00 9/1/2014 13:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00 9/1/2014 15:00		0.0 0.0 0.0 0.0 0.6 3.5 6.6 9.2 10.9 11.8 12.3 7.6 8.0 6.1 5.4 2.4 0.5 0.0	0.06 0.06 0.06 0.06 0.06 0.12 0.12 0.12 0.12 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.0	0.20 0.21 0.01 0.00 0.00 0.00 0.00 0.00	0 0.35 0 0.35 1 0.35 9 0.35 9 0.35 9 0.88 9 0.88 9 0.88 9 1.23 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 9 1.23 7 0.35 7 0.35	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00	0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.5 0.6 0.6 0.7 0.5 0.5 0.5 0.5 0.5 0.6 0.7 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 5.5.5 8.1 1 9.8 1 10.4 1 10.9 9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.8 8.1 9.8 10.4 10.9 6.2 6.5 4.6 4.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	97.7 97.7 97.7 97.7 97.7 97.7 97.7 97.7

Model starts September 1st

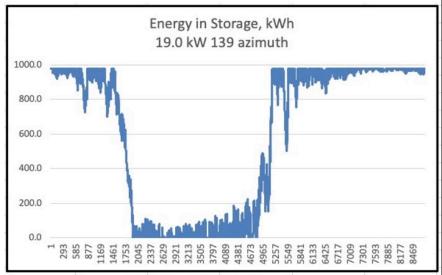
Results: Ten Cases Modeled

					PV	Grid
	1	Storage,	PV Used,	PV stored,	exported,	imported,
PV, kW	% load	gallons	kWh	kWh	kWh	kWh
19	100	0	7900	0	15025	15031
19	100	1000	7900	4381	10644	10445
19	100	2000	7900	5020	10005	9768
19	100	5000	7900	5276	9749	9491
19	100	10000	7900	5384	9641	9355
32.4	171	0	8629	0	30484	14302
32.4	171	1000	8629	5412	25072	8718
32.4	171	2000	8629	7131	23353	6907
32.4	171	5000	8629	7750	22734	6252
32.4	171	10000	8629	7899	22585	6089

The Winter Trough



1,000 Gallons (98 kWh) of Thermal Storage



10,000 Gallons (978 kWh) of Thermal Storage

Note that the vertical axis, kWh in storage, is ten times higher in the 10,000 gallon case.

Solar availability and high heating loads always produce the winter trough. The same result occurred on the solar thermal house in Hanover, NH – the tank dropped from peak temperature to minimum temperature for 6-8 weeks then bounces back up.

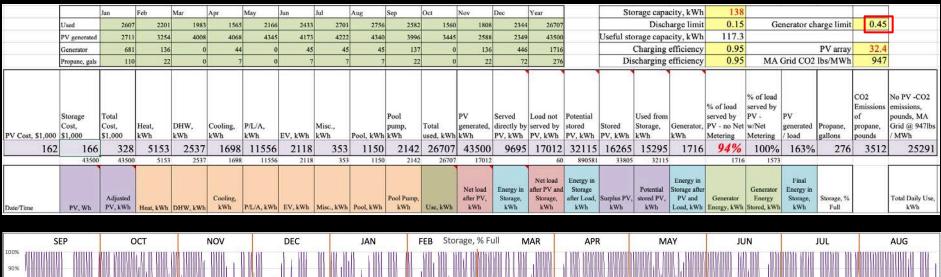
Add Electric Batteries

Thermal storage capacity, kWH					H 98 Thermal storage capacity, gallons H2O							1000	0	Storage temp high limi					12		37 P-2/27532876725356			3
					1										St	torage t	emp lo	w limit	8	35	kV	Wh/Batt	tery	13.5
											-1		Poot	f oreo E	V W/s	F	•			Rot	tery sto	rage k	W/h	40.5
	2000000000		-v-101 - Pakenton										175-500,000,000		2.72.0 S20.0050	_				_				thomponion
	PV	array 1	39, kW		19.0								1	055	13	Max 1	oof area	at 80% =	= 1824 sf	Cl	harging	efficie	ncy	95%
	PV	array 3	19 kW		0.0									0	13	8				Die	scharge	efficie	ncv	95%
	- 1	urray 5	17, 11,	4	0.0		175				_			v	,12,	9				Di	marge	CITICIC	110)	3570
		PV	001670	www.co.co.co.co.co.co.co.co.co.co.co.co.co.					1	Total non-	Grid energy imported serving non-	0134090	Non- heating use served		Grid energy into	Total imported grid	PV energy into thermal	PV energy	PV	Fraction of PV energy	in and out of Battery,	, after		
	6	generated, kWh			P/L/A, kWh	Laboration and the latest and the la	Heating, kWh			heating used, kWh	heating, kWh	Total load, kWh	directly by PV, kWh			energy, kWh	storage, kWh	exported, kWh	generation load	used on site	kWh, 95% efficiency			
		22925	702	702	6302	2 2118	13107			9824	5204	22931	4620	328	0 5241	10445	4381	10644	1 100%	79%	5756	4888		
N	4ax	15.0	0.1	0.5	1.3	3 1.7	5.7			2.7	13.3	8 14.9	4.6	5 14	.9 12.	7 14.	9 5.	7 10.	7 51.	1 13.	.0	Ť		
Т	otal	22925	702	702	630		13107			9824				3503										
Date/Time		PV, kWh	DHW. kWh	Cooling,	P/L/A, kWi	h EV, kWh	Heating,			Use except heating,	Surplus PV after Use except heating, kWh	Heating load, kWh	Surplus PV applied to heating load, kWh	Remaining heating load, kWh	storage,	Remaining heat load, kWh	Grid energy into heating kWh		Energy added to storage, kWI	Surplus PV exported to the grid,	Energy in Thermal Storage, kWh		Surplus PV stored in batteries, kWh	
9/1/2014 0:00		0.0	0.06	0.09	0.3		0.00	0.00	0.00	0.5	0.0	0.0	The same of the sa		.0 0.	0 0.	0.0	0.	-	-	.0 97.7	7		
9/1/2014 1:00		0.0	0.06	0.20	0.3		0.00	0.00	0.00						.0 0.									
9/1/2014 2:00		0.0	0.06	0.20	0.3		0.00	0.00	0.00						.0 0.									
9/1/2014 3:00		0.0	0.06	0.14	0.3		0.00	0,00	0.00						.0 0.									
9/1/2014 4:00		0.0	0.06	0.09	0.3		0.00	0.00	0.00						.0 0.									
9/1/2014 5:00 9/1/2014 6:00		0.6	0.12	0.09	0.33		0.00	0.00	0.00						0.0 0.0									
9/1/2014 7:00		6.6	0.12	0.09	0.8		0.00	0.00	0.00															
9/1/2014 8:00		9.2	0.12	0.09	0.88		0.00	0.00	0.00						.0 0.									
9/1/2014 9:00		10.9	0.12	0.09	0.88		0.00	0.00	0.00						.0 0.									
9/1/2014 10:00		11.8	0.06	0.09	1.2	3 0.00	0.00	0.00	0.00	1.4	10.4	4 0.0	0.0	0	.0 0.	0.	0.0	0.	0 0.	0 10.	.4 97.7	7		
9/1/2014 11:00		12.3	0.06	0.14	1.2	3 0.00	0.00	0.00	0.00	1.4	10.5	9 0.0	0.0	0	.0 0.	0.	0.0	0 0.	0 0.	0 10.	.9 97.7	7		
9/1/2014 12:00		7.6	0.06	0.14	1.2		0.00	0.00	0.00						.0 0.									
9/1/2014 13:00		8.0	0.06	0.19	1.2		0.00	0.00	0.00						.0 0.									
9/1/2014 14:00		6.1	0.06	0.19	1.2		0.00	0.00	0.00						.0 0.									
9/1/2014 15:00		5.4	0.06	0.19	1.2		0.00	0.00	0.00															
9/1/2014 16:00		2.4	0.06	0.23	1.2		0.00	0.00	0.00						0.0									
9/1/2014 17:00		0.5	0.12	0.28	0.88		0.00	0.00	0.00						0.0 0.0									
9/1/2014 18:00 9/1/2014 19:00		0.0	0.12 0.12	0.33	0.88		0.00	0.00	0.00						0.0 0.0								+	
9/1/2014 19:00		0.0	0.12	0.37	0.3		0.00	0.00	0.00						.0 0.									
9/1/2014 21:00		0.0	0.12	0.37	0.3		0.00	0.00	0.00															
9/1/2014 22:00		0.0	0.06	0.37	0.3		0.00	0.00	0.00															
9/1/2014 23:00		0.0	0.06	0.28	0.3		0.00	0.00	0.00														69.6	32.4

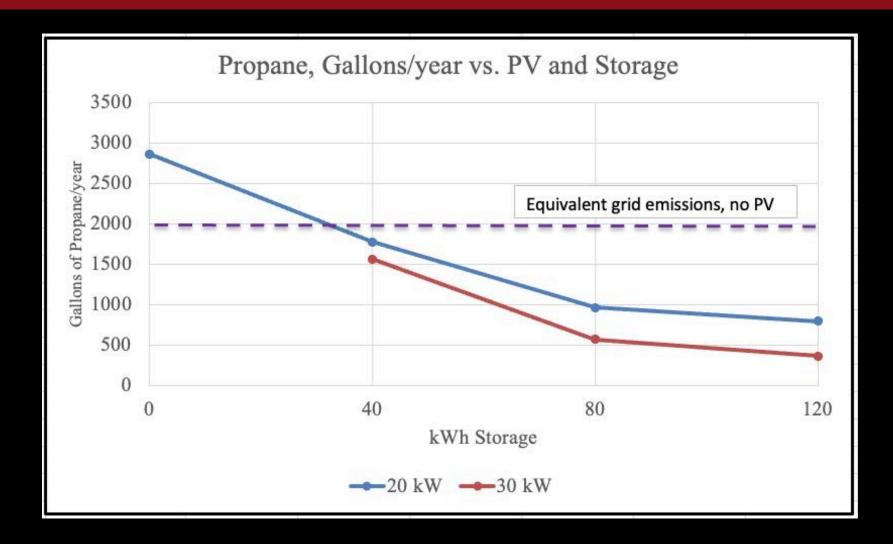
This is a simplified model on the battery side, likely overestimates the energy stored

An Off-grid House

- 4,400 sf house on Martha's Vineyard with a heated pool
- 32.4 kW PV; 138 kWh battery storage; propane generator
- Hourly model to optimize systems
- Systems design by Brice Delhougne Energylogik



An Off-grid House



Thank You!

